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S/055/59/000/06/15/027  
B006/B005

24.2200

AUTHORS:

Smol'kov, N. A., Grekov, V. M.

TITLE:

Some Properties of the  $\text{Li}_{2.0}^{\vee}\text{O} \cdot x\text{Fe}_{2.0}^{\vee}\text{O}_3$  System

PERIODICAL:

Vestnik Moskovskogo universiteta. Seriya matematiki, mekhaniki, astronomii, fiziki, khimii, 1959, No. 6, pp. 137 - 141

TEXT: Lithium ferrites of this type are very important in technology since their solid solutions with other ferrites form magnetic materials having a small tangens of the loss angle within a range of some tens of Mc/sec, and good time- and impulse characteristics. The crystal structure of these ferrites has been insufficiently investigated. A cubic lattice of the rock-salt type was found as well as a tetragonal modification - the transition point was found to be at  $660^{\circ}$ . The modification  $\text{Li}_{2.0}\text{O} \cdot \text{Fe}_{2.0}\text{O}_3$  has its transition point far below  $660^{\circ}$ . A phase with spinel structure was also found for ferrites with  $x = 2, 3, 4$ .  $\text{Li}_{2.05}\text{Fe}_{2.0}\text{O}_3$  has a spinel structure with  $a = 8.309$  or  $8.37$  Å. A number of further details taken from publications are mentioned. Subsequently, the authors present experimental results concerning the determination of the Curie point, and the static magnetic

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Some Properties of the  $\text{Li}_2\text{O} \cdot x\text{Fe}_2\text{O}_3$  System

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characteristics of ferrites ( $x = 1, 2, \dots, 6$ ).  $\theta_K$  was determined from the change in inductance of a ferrite-core coil on heating from  $-196$  to  $+700^\circ$ . Fig. 1 shows the dependence of the magnetic permeability  $\mu$  on  $H$  for all  $x$ -values, Fig. 2 the dependence of the primary and maximum permeability  $\mu_0$  and  $\mu_{\max}$ , and the coercive force  $H_c$  of ferrites, on their composition, Fig. 3 the dependence of the magnetic residual and maximum induction  $B_r$  and  $B_m$  of ferrites on their composition, and Fig. 4 the dependence of the angle of rotation  $\varphi$  of the polarization plane on  $H$ . Further, the authors investigated the high-frequency properties of ferrites. The Faraday effect was investigated at  $9370 \text{ Mc/sec}$  by the method published in Ref. 9. Fig. 5 shows the dependence of the angle of rotation of the polarization plane on the composition at  $H = \text{const}$  for three different temperatures. It is shown that the compound  $\text{Li}_2\text{O} \cdot 0.5\text{Fe}_2\text{O}_3$  is the most magnetoactive one in the range of superhigh frequencies. This compound also shows the smallest coercive force, and maximum values of  $\mu_0$  and  $\mu_{\max}$ ,  $B_r$  and  $B_m$ , and  $\varphi$ . A device for measuring the phase shift  $\Delta\varphi$  and the damping  $\delta$  of electromagnetic waves passing through a ferrite plate is described (Fig. 6). If  $Q = \Delta\varphi/\delta$  is defined as the quality factor of ferrite, the compound with  $x = 5$  also has the maximum

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Some Properties of the  $\text{Li}_2\text{O} \cdot x\text{Fe}_2\text{O}_3$  System

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Q-value as is shown by Fig. 7. There are 7 figures, 1 table, and 20 references, 4 of which are Soviet.

ASSOCIATION: Kafedra magnetizma (Chair of Magnetism)

SUBMITTED: January 22, 1959

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69164

24,7900

S/139/59/000/06/022/034  
E201/E191

AUTHORS: Smol'kov, N.A., and Day Do-shen

TITLE: Some Properties of Yttrium and Gadolinium Ferrite Garnets

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy, Fizika,  
1959, Nr 6, pp 145-151 (USSR)

ABSTRACT: The authors measured the static (d.c.) magnetic properties and high-frequency magnetic and dielectric properties of two garnet ferrites: yttrium ferrite ( $3\text{Yt}_2\text{O}_3 \cdot 5\text{Fe}_2\text{O}_3$ ), which has not a compensation point, and gadolinium ferrite ( $3\text{Gd}_2\text{O}_3 \cdot 5\text{Fe}_2\text{O}_3$ ) which has a compensation point. The compensation point is a temperature,  $T_{\text{comp}}$ , at which the saturation magnetization,  $M_s$ , becomes zero. Samples were prepared by the usual ceramic techniques from  $\text{Fe}_2\text{O}_3$ ,  $\text{Yt}_2\text{O}_3$  and  $\text{Gd}_2\text{O}_3$ . The samples were subjected to a pressure of 3 tons/cm<sup>2</sup> and were fired for 3 hours at 1300 °C in air. Yttrium garnet had a Curie point  $\theta_K$  at 287 °C; gadolinium garnet at  $\theta_K = 291$  °C and a compensation point at  $T_{\text{comp}} = 14$  °C. Some of the results are given in Figs 1 (Yt garnet) and 2 (Gd garnet). These figures show the

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temperature dependences of the initial ( $\mu_0$ ) and maximum ( $\mu_{\max}$ ) permeabilities, coercive force ( $H_c$ ), residual induction ( $B_r$ ) and maximum induction ( $B_m$ ) reached in maximum fields of  $H = 40$  Oe produced by windings on the ferrite toroids.  $B_m$  and  $B_r$  of both ferrites fall monotonically with temperature, in agreement with Pauthenet's observations (Refs 2, 8, 9). The temperature dependences (between  $-200$  and  $+300$  °C) of  $\mu_0$ ,  $\mu_{\max}$  and  $H_c$  of Yt garnet have the form usual for ferro-magnetics without a compensation point (Fig 1); the same dependences of Gd garnet (Fig 2) are anomalous because of the presence of  $T_{\text{comp}}$ . This anomaly can be explained as follows. The saturation magnetization  $M_s$  of Gd garnet falls, starting at  $-196$  °C, and reaches zero at  $T_{\text{comp}} = 14$  °C, and consequently the permeabilities decrease to  $\mu_0 = \mu_{\max} = 1$  and the coercive force  $H_c$  rises from 5 Oe at  $-196$  °C to 21.8 Oe at 14 °C. The value of  $H_c$  at  $T_{\text{comp}}$  was obtained as the point of intersection of the curves  $H_c = f(T)$  obtained at temperatures lower and higher than  $T_{\text{comp}}$ . The rise of

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$H_c$  is mainly due to the fall in  $M_s$ . On heating above  $T_{comp}$  the value of  $H_c$  decreases first very sharply (in the region where  $M_s$  rises) and then it falls more slowly. The permittivities  $\mu_0$  and  $\mu_{max}$  rise above  $T_{comp}$ , reaching their maximum values at the Curie point. Polder (Ref 19) and Hogan (Ref 20) showed that a high-frequency magnetic field  $h$  and the resultant induction  $b$  in a medium magnetized to saturation along the OZ-axis are related by a tensor expression

$$b = T_{ij}h, \quad (1)$$

where  $T_{ij}$  is the permeability tensor:

$$T_{ij} = \begin{vmatrix} \mu & -iK & 0 \\ +iK & \mu & 0 \\ 0 & 0 & \mu_z \end{vmatrix} \quad (2)$$

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In Eq (2) the tensor components are  $\mu = \mu' - i\mu''$ ,  $K = K' - iK''$ ,  $\mu_z = \mu'_z - i\mu''_z$ . From these tensor

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components the effective complex permeability  $\mu_{\perp}$  can be found using:

$$\mu_{\perp} = u'_{\perp} - iu''_{\perp} = \frac{\mu^2 - K^2}{\mu} \quad (3)$$

Employing the technique developed by Vasil'yev (Ref 21) the authors determined the components of  $T_{ij}$ , the complex effective permeability  $\mu_{\perp}$  and the complex permittivity  $\epsilon = \epsilon' - i\epsilon''$  of both ferrites at 9370 Mc/s; the results are given in Figs 3-8. Figs 3 and 4 give dependences of  $\mu_z$ ,  $\mu'_{\perp}$  and  $\mu''_{\perp}$  on the magnetizing field  $H$  (up to 2000 Oe) at three temperatures: +16, +130 and +200 °C for Yt garnet (Fig 3) and +45, +130 and +200 °C for Gd garnet (Fig 4). With increase of the field  $H$  the magnitude of the real part of the effective permeability  $\mu'_{\perp}$  decreases, due to its dispersion nature, in agreement with Pauthenet's theory (Ref 19). It can be shown theoretically that when  $H$  is fixed, the value of  $\mu'_{\perp}$  rises on decrease of  $M_s$ , and conversely. The experimental results obtained by the

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authors (Figs 3-6) confirm this (Figs 5 and 6 show the temperature dependences of  $\mu'_1$  and  $\mu''_1$  of Yt and Gd garnets respectively between 0 and 200 °C). For Yt garnet the value of  $\mu'_1$  rises on increase of temperature from +16 to +200 °C, while for Gd garnet the value of  $\mu'_1$  falls between +45 and +130 °C, since  $M_s$  rises in this region (cf. Fig 2). On further heating between +130 and 200 °C the real part of permeability of Gd garnet rises, because  $M_s$  falls at these temperatures. Values of  $\mu'_z$  of both garnets are practically independent of the applied field (Figs 3, 4). The results for  $\mu'_1$  and  $\mu'_z$  are in agreement with those obtained by Nemerich and Cacheris (Ref 16) for yttrium ferrite garnet and for MgMn and Ni ferrites. The imaginary part of permeability  $\mu''_1$ , which represents effective magnetic losses, rises in both garnets with increase of the field H, indicating approach to ferromagnetic resonance (Figs 3, 4), and falls on increase of temperature (Figs 5, 6). The value of  $\mu''_z$  could not be determined because of its low value. Fig 7 gives dependence of the real and imaginary parts of

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the tensor components  $\mu$  and  $K$  on the field  $H$  (up to 2000 Oe) for Yt garnet: these curves show that  $\mu'$  falls with increase of  $H$ , and  $K'$ ,  $\mu''$ ,  $K''$  all rise with increase of  $H$ . Measurements on Gd garnet showed that  $\mu' = \mu'_1$ ,  $\mu'' = \mu''_1$  and  $K = 0$ . Fig 8 represents

the temperature dependences of the real ( $\epsilon'$ ) and imaginary ( $\epsilon''$ ) parts of permittivity of both garnets between 0 and 200 °C. All these quantities are practically independent of temperature:  $\epsilon' = 6-7$ , as in spinel-type ferrites, and dielectric losses, represented by  $\epsilon''$ , are very low (0.001-0.002).

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There are 8 figures and 21 references, of which 1 is Soviet, 13 English, 5 French, 1 translation from French into Russian and 1 international.

ASSOCIATION: Moskovskiy gosuniversitet imeni M.V. Lomonosova  
(Moscow State University imeni M.V. Lomonosov)

SUBMITTED: January 28, 1959

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24. 2200

67686

SOV/126-8-4-8/22

AUTHORS: Smol'kov, N.A., and Gushchina, S.A.

TITLE: Nickel-Cadmium Ferrites  $\gamma^1$

PERIODICAL: Fizika metallov i metallovedeniye, 1959, Vol 8, Nr 4,  
pp 557-561 (USSR)

ABSTRACT: The authors made ferrites of eleven compositions by a ceramic method with the general formula  $Ni_{1-x}Cd_xFe_2O_4$ , where x varies from 0 to 1 in 0.10 intervals. The basic raw materials were the higher oxides  $Fe_2O_3$  and  $CdO$  of the "ChDA" class and the lower nickel oxide  $NiO$  of the "Ch" class. The specimens were pressed at a pressure of 3 t/cm<sup>2</sup>. In order to obtain material with high magnetic properties, the charger after milling, drying and sieving was given a preliminary annealing at 950 °C for 3 hours, and was then ground again and mixed with a plasticizer (polyvinyl alcohol). From the pressed powder specimens were made which were annealed at 1245 °C for 3 hours. Specimens made without preliminary annealing exhibited low magnetic properties. The Curie point  $O_k$  of the ferrites was determined by the fall in induction of a ferrite core-coil on heating, and the static properties (initial and

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Nickel-Cadmium Ferrites

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maximum magnetic permeabilities,  $\mu_0$  and  $\mu_{\max}$ , coercive force  $H_c$ , residual and maximum magnetic inductions,  $B_r$  and  $B_m$ ), were measured in toroidal specimens by means of a ballistic instrument. The results of measurements of the above properties in relation to composition are shown in Figs 1-4. By means of an earlier described method (Ref 8) the authors studied the Faraday effect in cylindrical ferrite specimens of 55 mm length and 5 mm diameter at room temperature at a frequency of 9370 megahertz. Fig 5 shows a curve for the dependence of the angle of rotation of the polarisation plane  $\varphi$  of  $Ni_{1-x}Cd_xFe_2O_4$  ferrites at a fixed magnetising field  $H$  of 460 oersted, on composition. Simultaneously the high frequency quality  $Q$  of ferrites was determined at a fixed magnetising field of  $H = 600$  oersted. The measurements were carried out on plate-like ferrite needles, 3 x 7.5 x 95 mm, by means of an apparatus, the layout of which is shown in Fig 6. In this apparatus the phase shift  $\Delta\varphi$  and the damping  $\delta$  (in decibels) ✓

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Nickel-Cadmium Ferrites

were determined and from the results obtained the high frequency quality  $Q = \Delta\varphi/\delta$  was calculated. In Fig 7 the dependence of  $Q$  of the  $Ni_{1-x}Cd_xFe_2O_4$  on composition at a frequency of 9370 megahertz at a fixed magnetisation field of  $H = 600$  oersted, is shown. The authors arrive at the following conclusions. In solid solutions of nickel and cadmium ferrites the Curie point decreases steadily with increase in the concentration of cadmium ferrite in the solution, the initial and maximum magnetic permeabilities increase, reaching a maximum in the range of 60% cadmium ferrite concentration and then fall sharply; the coercive force attains a minimum for a composition of 50% cadmium ferrite; the residual and maximum magnetic inductions attain a maximum in the range of 20% cadmium ferrite concentration; the compositions  $Ni_{0.9}Cd_{0.1}Fe_2O_4$  and  $Ni_{0.8}Cd_{0.2}Fe_2O_4$  have maximum values of angle of rotation of the polarisation plane  $\varphi$  and high frequency quality  $Q$ .

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There are 7 figures and 8 references, of which 6 are Soviet, 1 is French and 1 is European (S. Ceram. Ind.) 4

Nickel-Cadmium Ferrites

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SOV/126-8-4-8/22

ASSOCIATION: Moskovskiy gosudarstvennyy universitet  
imeni M.V. Lomonosova  
Card 4/4 (Moscow State University imeni M.V. Lomonosov)

SUBMITTED: February 12, 1959

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SMOL'KOV, N.A.

Properties of copper cadmium ferrates. Vest Mosk. un. Ser. nat.,  
mekh., astron., fiz., khim. 14 no.2:85-91 '59 (MIRA 13:3)

1. Kafedra magnetizma Moskovskogo gosuniversiteta.  
(Copper cadmium ferrates)

SMOL'KOV, N.A.; YEREMKINA, V.A.

Effect of magnesia aluminate on the properties of magnesium  
ferrate. Vest Mosk. un. Ser. mat., mekh., astron., fiz., khim.  
14 no.2:93-99 '59 (MIRA 13:3)

1. Kafedra magnetizma Moskovskogo gosuniversiteta.  
(Magnesium aluminates) (Magnesium ferrate)

1. (3)

AUTHORS:

Smol'kov, N. A., Simonov, Yu. P.

SOV/46-23-3-7/34

TITLE:

Properties of Solid Solutions  $\text{NiFe}_2\text{O}_4$  -  $\text{MgFe}_2\text{O}_4$   
(Svojstva tverdykh rastvorov  $\text{NiFe}_2\text{O}_4$  -  $\text{MgFe}_2\text{O}_4$ )

PERIODICAL:

Izvestiya Akademii nauk SSSR. Seriya fizich. i khim. 1959,  
Vol 23, Nr 3, pp 307-310 (USSR)

ABSTRACT:

In the present paper the authors investigate structural, magnetic, and high-frequency properties of the nickel-magnesium-ferrites of stoichiometric composition. The samples were produced from oxides by a sintering of 5 hours at  $1500^\circ$ . The molecular weights and the colors of the solutions are given in the table. The values found for the constants of the crystal lattice of the solutions are:

solution Nr	lattice constant a in Å
1	$3.321 \pm 0.001$
2	$3.328 \pm 0.001$
3	$3.341 \pm 0.001$
4	$3.349 \pm 0.001$
5	$3.362 \pm 0.001$

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Properties of Solid Solutions  $\text{NiFe}_2\text{O}_4$  -  $\text{MgFe}_2\text{O}_4$

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In figure 1 the curve of dependence of the value  $\alpha$  on the  $\text{MgFe}_2\text{O}_4$ -content in the solution is given. The absolute values  $\alpha$  of the solutions proved to be slightly lower than those given in reference 6:

$\text{NiFe}_2\text{O}_4$  - 8.34 kX;  $\text{MgFe}_2\text{O}_4$  - 8.37 kX.

In order to determine the type of the spinels of the solutions investigated the relations of the line intensity  $I_{400}/I_{422}$  under consideration of the absorption-, polarization- and the Lorentz factor were determined (Fig 2) by means of tables (Ref 8). The values of  $I_{400}/I_{422}$  which were experimentally found and entered in the diagram show within the possible error limits in the photoprocess and in the measurement by means of the photometer that the solid solutions in the system  $\text{NiFe}_2\text{O}_4$  -  $\text{MgFe}_2\text{O}_4$  have the structure of an inverse spinel. As was demonstrated already earlier the Curie point  $\theta_K$  of the solid solutions decreases linearly from  $585^\circ$  for nickel ferrite, to  $325^\circ$  for magnesium ferrite.

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Properties of Solid Solutions  $\text{NiFe}_2\text{O}_4$  -  $\text{MgFe}_2\text{O}_4$

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In figure 3 the dependences of the initial and the maximum magnetic permeability  $\mu_n$  and  $\mu_{\max}$  on the composition and in figure 4 the curves of the coercive force  $H_c$ , of remanent induction  $B_r$  and of the maximum induction  $B_{\max}$  are given. As may be seen  $\mu_n$ ,  $\mu_{\max}$ ,  $B_r$  and  $B_{\max}$  decrease monotonously at a higher magnesium-ferrite-concentration in solution whereas  $H_c$  first increases until the solution  $\text{Ni}_{0.5}\text{Mg}_{0.5}\text{Fe}_2\text{O}_4$  is attained and then practically remains unchanged. The Faraday effect was investigated according to the method described earlier (Refs 9 .. 10). The curves of dependence of the rotation angle of the polarization plane  $\varphi$  and the high-frequency losses  $\delta$  on the composition are shown in figure 5. From these curves it may be seen that the angle monotonously decreases with the increase of the magnesium-ferrite content in solution while the losses  $\delta$  have their minimum at  $\text{Ni}_{0.75}\text{Mg}_{0.25}\text{Fe}_2\text{O}_4$ . The reduction of the  $\varphi$ -angle may be caused by the fact that the saturation magnetization of the solutions decreases from nickel to magnesium-ferrite.

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Properties of Solid Solutions  $\text{LiFe}_2\text{O}_4 - \text{MgFe}_2\text{O}_4$

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There are 5 figures, 1 table, and 10 references, 5 of which are Soviet.

ASSOCIATION: Kafedra magnitizma fizicheskogo fakul'teta i kafedra neorganicheskoy khimii khimicheskogo fakul'teta Moskovskogo gos. universiteta im. M. V. Lomonosova (Chair of Magnetism of the Physics Department and Chair of Inorganic Chemistry of the Chemical Department of the Moscow State University im. M. V. Lomonosov)

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24(3)

AUTHORS:

Smol'kov, N. A., Belov, V. F.

SOV/48-23-3-15/34

TITLE:

Several Properties of Ferrites Under Pulse Conditions (Nekotoryye svoystva ferritov v impul'snom rezhime)

PERIODICAL:

Izvestiya Akademii nauk SSSR. Seriya fizicheskaya, 1959, Vol 23, Nr 3, pp 357-360 (USSR)

ABSTRACT:

The pulse device shown in figure 1 as a block diagram was used in the present investigation for examining the duration of magnetic reversal. The duration of magnetic reversal was visually read from the width of the signal appearing on the screen of the synchroscope. Figure 2 shows the isothermal lines

$H_m = f\left(\frac{1}{\tau}\right)$  for industrial ferrite Nr 1, which is used in computers. Figure 3 gives the temperature dependences  $H_0$  and  $S_w$ .

$H_0$  denotes the value of the threshold field,  $S_w$  the coefficient of magnetic reversal. In the case of rising temperature the two values decrease. This may be due to the decrease of the elastic tensions and the reduction of the anisotropy constant

in the material. The isothermal lines  $H_m = f\left(\frac{1}{\tau}\right)$  for

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Several Properties of Ferrites Under Pulse Conditions SOV/48-23-3-15/34

ferrite Nr 2 are given in figure 4. Ferrite Nr 2 was produced by sintering the oxides at  $1,300^{\circ}$  and subsequent tempering. The composition is  $MgO.3MnO.3Fe_2O_3$ . Figure 5 shows the temperature dependence of the threshold field and of the coefficient of magnetic reversal of ferrite Nr 2. The curves indicate the maximum value of the threshold field to be in the range of  $-117^{\circ}$ . Such an anomaly is likely to be due to the existence of phase transitions taking place in some ferrites. Figures 2 and 4 show that the range of linear dependence  $H_m = f\left(\frac{1}{\tau}\right)$  is in the case of ferrite Nr 1 in weaker fields than in the case of ferrite Nr 2 and that consequently ferrite Nr 1 is more economical.  $H_m$  denotes the external field,  $\tau$  the duration of magnetic reversal. There are 5 figures and 15 references, 2 of which are Soviet.

ASSOCIATION: Kafedra magnetizma fizicheskogo fakul'teta Moskovskogo gos. universiteta im. M. V. Lomonosova (Chair of Magnetism of the Physics Department of Moscow State University imeni M. V. Lomonosov)

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24(3)

307/43-23-5-18/34

AUTHORS: Smol'kov, N. A., Fomenko, Ye. I.

TITLE: Some Properties of Ferrites at Super High Frequencies (Nekotoryye svoystva ferritov na sverkhvysokikh chastotakh)

PERIODICAL: Izvestiya Akademii nauk SSSR. Seriya fizicheskaya, 1959, Vol 23, Nr 3, pp 377-379 (USSR)

ABSTRACT: As Polder (Ref 1) has theoretically shown, a high-frequency plane-polarized electromagnetic oscillation is decomposed into two waves when passing through a magnetized ferromagnetic: one wave is left handed circularly polarized and one right-handed. The velocities of propagation in both waves are different. For this reason the resulting plane-polarized wave which emerges from the ferromagnetic shows a rotation of the polarization plane by  $\varphi$  (compared to the incident wave) - i.e. a Faraday effect may be observed which is similar to the optical one. Roberts (Ref 2) and Hogan (Ref 3) proved this experimentally with ferrites. Six diagrams are discussed. In the first diagram the rotation of the polarization plane in dependence of the external magnetic field H in a cylindrical magnesium-manganese-ferrite sample ( $\text{Mg}_{0.75}\text{Mn}_{0.25}\text{Fe}_2\text{O}_4$ )

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Some Properties of Ferrites at Super High Frequencies

at a frequency of 9350 Megacycles is shown. In the second diagram the same is demonstrated for magnesium-nickel-manganese-ferrite. In the diagram 3a the damping of the polarized wave is shown in dependence of the external magnetic field ( $\gamma$  has a sharp maximum), and in 3b the dependence of the ellipticity on the external magnetic field is shown; d shows a minimum at the same place where  $\gamma$  has its maximum. The fourth diagram shows the dependence of the rotation of the polarization plane on the external magnetic field  $H$  for 6 different magnesium-manganese-ferrites. In the fifth diagram the angle of rotation of the polarization plane is shown for three different temperatures as a function of the mixing proportion between  $MnFe_2O_4$  and  $MgFe_2O_4$  at a field strength of  $H_0 = 460$  Oe. There are 5 figures and 9 references, 3 of which are Soviet.

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S/196/62/000/020/006/021  
E194/E155

AUTHORS: Pakhomov, A.S., and Smol'kov, N.A.

TITLE: Ferrites. Their structure and certain physical properties

PERIODICAL: Referativnyy zhurnal, Elektrotehnika i energetika, no.20, 1962, 3, abstract 20 B 14. (In collection: 'Antiferromagnetizm i ferrity' ("Antiferromagnetism and ferrites"), M., AN SSSR, 1962, 119-213).

TEXT: Recent experimental and scientific observations of the crystalline structure and certain properties of ferrites are systematically presented, in three chapters. The first considers the detailed structure and properties of different crystalline lattices (structure of spinel, garnet, magnetoplumbite, rock salt, etc), the relationship between structure and sintering conditions and the composition of the initial charge, and also the crystal chemistry of ferrites. The second chapter presents the theory of magnetism of ferrites, the semi-classical theory of Néel, the theory of Yafet and Kittel (the generalised Néel's theory), and quantum theory. The third chapter, occupying half the total  
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Ferrites. Their structure and ...

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article, deals with the physical properties (thermal, magnetic and electric) of ferrites. Experimental data are given about the presence of conversion points in ferrites which accompany the occurrence of peaks on the temperature curves of specific heat and coefficient of thermal expansion. Calculations of molecular magnetic moments of saturation of ferrites with spinel and garnet lattice on the basis of Néel's theory are made and compared with experimental results, and discrepancies are discussed. The magnetic properties of mixed ferrites with spinel, garnet and magnetoplumbite structure are considered. The influence of the sintering conditions (sintering temperature, atmosphere, method of cooling) on the static magnetic characteristics and their temperature relationships are shown. The constants of magnetic anisotropy of single crystals of different ferrites are tabulated and their dependence on the concentration of  $Fe^{3+}$  ions in the spinel lattice and on the concentration of Co ions in Ferroxlana\* is examined. Finally, the article examines the electrical conductivity of ferrites. 41 illustrations, 303 references.

\* Ferroxlana is a trade name (Philips, of Eindhoven).

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L 13104-66 EWT(m)/EWP(t)/EWP(b) IJP(c) JD/JG

ACC NR: AP5025794

SOURCE CODE: UR/0363/65/001/009/1564/1565

AUTHOR: Smol'kov, N. A.; Dobrovol'skaya, N. V.

ORG: All-Union Scientific Research Institute of Mineral Raw Materials  
(Vsesoyuznyy nauchno-issledovatel'skiy institut mineral'nogo syr'ya)

TITLE: Magnetic susceptibility of lanthanum, neodymium, and gadolinium  
oxides

SOURCE: AN SSSR. Izvestiya. Neorganicheskiye materialy, v. 1, no. 9,  
1954, 1564-1565

TOPIC TAGS: lanthanum oxide, neodymium oxide, gadolinium oxide, mag-  
netic susceptibility, paramagnetism, diamagnetism, magnetic moment

ABSTRACT: The magnetic susceptibility  $\chi$  of the oxides  $\text{La}_2\text{O}_3$ ,  $\text{Nd}_2\text{O}_3$ ,  
and  $\text{Gd}_2\text{O}_3$  was measured by the Faraday method at temperatures of 20-800°C.  
 $\text{La}_2\text{O}_3$  has a constant diamagnetic susceptibility  $\chi_{\text{diam}} = -0.23 \cdot 10^{-6} \text{ cm}^3$   
 $\text{g}^{-1}$  over the entire temperature range.  $\text{Nd}_2\text{O}_3$  is paramagnetic but its  
temperature dependence deviates from the Curie-Weiss law particularly  
at high temperatures; this is due to the effect of the energy levels of  
the lower multiplet which are located above the ground state  $^4I_{9/2}$  and

UDC: 546.65'221

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L 13104-66

ACC NR: AP5025794

whose contribution to the paramagnetism increases with  $T$ . The experimental effective magnetic moment of the  $\text{Nd}^{3+}$  ion is (in Bohr magnetons)  $\mu_{\text{eff}} = 3.79$  (theoretical value 3.68) for the free ion and 3.67 for the interacting ion. The susceptibility of  $\text{Gd}_2\text{O}_3$  conforms rigorously the Curie-Weiss law because the paramagnetism of  $\text{Gd}^{3+}$  is due solely to the magnetic moment of the ion in the ground state  $^8S_{7/2}$ .  $\chi_{\text{para}} = 140 \cdot 10^{-6}$

$\text{cm}^3 \text{g}^{-1}$  at  $20^\circ\text{C}$ . Experimental  $\mu_{\text{eff}}$  for  $\text{Gd}^{3+}$  (in Bohr magnetons) is 7.95 (theoretical value 7.94). Orig. art. has: 2 figures, 1 formula.

SUB CODE: 07/ SUBM DATE: 16Apr65/ ORIG REF: 000/ OTH REF: 002

20/

Card 2/2

SMOL'KOV, V., kand.filosofskikh nauk

Socialist competition is the general feature of our social  
development. Komm.Vooruzh.Sil 3 no.24:8-16 D '62. (MIRA 15:12)

(Russia--Armed forces) (Socialist competition)

SOLOV'EV, V. G.

Dissertation defended for the degree of Candidate of Philosophical Sciences  
at the Institute of Philosophy 1962

"Socialist Competition -- A Principle of the Development of the Soviet Society."

Vestnik Akad. Nauk, No. 4, 1963, pp 119-145

USSR/Zooparasitology. Parasitic Worms. Helminths of Men.

G

Abs Jour: Ref Zhur-Biol., No 17, 1958, 76990.

Author : Smol'kov, V. T.

Inst :

Title : A Case of Simultaneous Echinococcosis of the Heart  
and Spleen.

Orig Pub: Zdravookhr. Kazakhstan, 1957, No 10-11, 109-110.

Abstract: No abstract.

Card : 1/1

SMOL'KOV, V.T.

Two cases of abdominal pregnancy diagnosed as tumor of the abdominal cavity. Zdrav. Kazakh. 22 no.2:75-76 '62. (MIRA 15:4)

1. Iz 1-oy Ust'-Kamenogorskoy gorodskoy bol'nitsy.  
(PREGNANCY, EXTRA-UTERINE) (ABDOMEN--TUMORS)



SMOL'KOV, V.T.; BABAYTSEV, V.A.; PISMAREV, V.V.

Analysis of sudden death in the home. Zdrav. Kazakh. 22  
no.5:46-48 '62. (MIRA 15:6)

1. Iz Vostochno-Kazakhstanskogo oblastnogo byuro sudebno-  
meditsinskoy ekspertizy.  
(UST'-KAMENOGORSK--DEATH--CAUSES)

BERKA, A.; SMOLKOVA, E.; BOGANOVSKI, E.

Indirect gasometric determination of urotropin. Cesk. farm.  
13 no.3:96-99 Mr'64.

1. Katedra analytické chemie KU, Praha.

\*

ACC NR: AP7001392

(A)

SOURCE CODE: UR/0413/66/000/021/0061/0061

INVENTORS: Smol'kova, V. S.; Yemel'yanov, N. M.; Yampol'skaya, E. G.; Smirnova, I. A.

ORG: none

TITLE: A method for obtaining an electrode paste for lead batteries. Class 21, No. 187857

SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 21, 1966, 61

TOPIC TAGS: lead, storage battery, urea, battery

ABSTRACT: This Author Certificate presents a method for obtaining an electrode paste for lead batteries. The paste is based on lead powder and is deposited on plates and dried. To increase the capacity of the battery, the lead powder is mixed with urea. To this dry mixture rubber cement is added. The amount of urea introduced may range from 3 to 20%.

SUB CODE: 10/ SUBM DATE: 24May63

Card 1/1

UDC: 621.3.035.4

CZECHOSLOVAKIA

SMOLKOVA, E; KRISTOFIKOVA, L; FELTL, L; GRUBNER, O

1. Institute of Physical Chemistry, Czechoslovak Academy of Sciences, Prague (for Grubner); 2. Institute of Analytical Chemistry, Charles University, Prague (for others)

Prague, Collection of Czechoslovak Chemical Communications, No 2, February 1966, pp 450-456

"Determination of the surface of powdery substances by the method of thermal desorption, using organic vapors as the sorbates."

SMITH, J. L.

Microbial "reserve" cells in the mucous membrane of the cervix  
Izv. Trudy KirgNOAGE no. 2163-64 '65.

(MIRA 18:11)

I. iz kafedry patologicheskoy anatomii (zav. - prof. B.F. Malyshev)  
Kirgizskogo gosudarstvennogo meditsinskogo instituta.

MIKHEYEVA, O.N.; ZHABRONOVA, Z.A.; POPOVA, L.A.; KAMENSKIY, I.N. [deceased];  
BEL'KIND, M.G.; TSVELEVA, I.A.; SMOL'NAYA, L.M.; KADYKOVA, N.F.;  
KASHITSYNA, A.D.

Biosynthesis of tetracycline on enriched media. Med.prom. 14  
no.1:31-34 Ja '60. (MIRA 13:5)

1. Moskovskiy zavod meditsinskikh preparatov No.1 i Vsesoyuznyy  
nauchno-issledovatel'skiy institut antibiotikov.  
(TETRACYCLINE)

Smolnický, T.

**AUTHORS:**

Mástar, P. and Smolnický, T.  
 Hemoglobin II. A Note on the Problem of Similarities  
 in the Structures of the Protein Component of Horse and  
 Human Hemoglobin. Preliminary Communication  
 (O hemoglobine II. K otázce podobnosti v struktuře  
 bílkovinné složky l'usko a konského hemoglobinu)  
 PRIONICAL: Chemické Listy 1958, Vol. 52(82), Nr. 10, pp 1991-1992  
 (Czechoslovakia) - 2 plates.

**TITLES:**

**ABSTRACT:**

It was considered that the non-specific hydrolysis of  
 haemoglobin by hydrochloric acid was responsible for  
 the small number of arginine and histidine peptides.  
 Trypsin hydrolysis was chosen because of its  
 specificity. Trypsin, purified by repeated  
 crystallization, was used at pH 7.5 (30 C, 24 hours).  
 Paper chromatography was used to separate the acid-  
 water (30:20:60) and the water-soluble (30:20:60) and paper  
 electrophoresis (pyridine-acetic acid: 10:1) and paper  
 40 V/cm; 2 hours) were used to study the products of  
 hydrolysis. The eluates from paper electrophoresis  
 were also prepared for study. Although fairly closely  
 related in structure, they differed mainly in those  
 peptides containing histidine (Pauly reagent used for

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location). Although there are 33 histidine residues  
 few were found in peptide form in the hydrolysates and  
 it is suggested that they play a role in the formation  
 of the complex with haem and in the reversible  
 bonding of oxygen in the haemoglobin molecule.  
 There are 4 figures, 11 references, 6 of which are  
 Czech and 5 English.

**ASSOCIATION:** Biochemický ústav, lékařská fakulta, Komenského  
 univerzity, Praha (Biochemistry Department, Medical  
 Faculty, Comenius University, Prague)  
**SUMMITTED:** April 14, 1958

Card 2/2

MASIAR, P.; SMOLNICKY, T.

On hemoglobin. Part 14 : Investigation on the neutral and weakly basic fraction of the tryptic digest of human and horse hemoglobin by chromatography on zerolit 225 and high-voltage electrophoresis. Coll Cz Chem 27 no.8:2018-2019 Ag '62.

1. Department of Biochemistry, P.J. Safarik University, Kosice.



SMOL'NIK, A.Yu., inzh.

Automatic control system of the main engine on the motorship  
"Kirovsk". Sudostroenie 39 no.9:40-44 S '62.

(MIRA 17:11)

SMOLNIK, Yu.Ye.; YAMCHENSKIY, N.G.; GUSENKO, V.I.

Application of mechanical vibrations in the oxidation of technical  
paraffins to synthetic fatty acids. Khim. i tekhn.topl. i masel  
10 no.11:26-28 N '65.

(MIRA 19:1)

1. UkrNigiproneft'.

SMOL'NIKOV, A.

*Our chapter in the book of the Revolution.*

Our chapter in the book of the Revolution. IUn.tekh. 3 no.10:  
3-7 0 '58. (MIRA 11:11)

(Communist Youth League)

SMOL'NIKOV, B.A.

Calculating natural vibrations of a closed frame system with a  
cyclic symmetry. Trudy LPI no.210:213-219 '60. (MIRA 13:11)  
(Structural frames--Vibration)

ACCESSION NR: AP4013391

S/0040/64,028/001/0171/0174

AUTHOR: Smol'nikov, B. A. (Leningrad)

TITLE: Motion of a solid body under the influence of the rotation of an internal flywheel

SOURCE: Prikladnaya matematika i mekhanika, v. 28, no. 1, 1964, 171-174

TOPIC TAGS: solid body, rotation, flywheel, nonsymmetric body, pure rotation, moment of inertia, kinetic moment

ABSTRACT: The author investigates the solution of the problem of finite rotation of a nonsymmetric solid body under the influence of the rotation of an internal flywheel whose axis is arbitrarily fixed in the body. He shows that in the general case of rotation of a flywheel about an arbitrary axis the carrying body performs pure rotation about another axis, called the concomitant axis. He derives formulas for determining the axis of the flywheel in the body according to a given magnitude of spatial rotation of the carrying body. Orig. art. has: 30 formulas and 1 diagram.

Card 1/2

ACCESSION NR: AP4013391

ASSOCIATION: none

SUBMITTED: 16Oct63

DATE ACQ: 26Feb64

ENCL: 00

SUB CODE: PH

NO REF SOV: 002

OTHER: 000

Card 2/2

ACCESSION NR: AP4043292

S/0040/64/028/004/0725/0734

AUTHOR: Smol'nikov, B. A. (Leningrad)

TITLE: Optimal modes of braking the rotary motion of a symmetrical body

SOURCE: Prikladnaya matematika i mekhanika, v. 28, no. 4, 1964, 725-734

TOPIC TAGS: jet motor, optimal operational mode, rotary motion, Pontryagin maximum principle, symmetrical body motion braking, time optimal problem

ABSTRACT: Control of the rotary motion of a solid, symmetrical body about its center of mass by means of nozzle-type jet engines is studied. Determination of two modes of operation of jet engines is considered: a) braking the velocity of the body in the shortest time (the expenditure of fuel is not given) and b) braking the velocity with minimal fuel expenditure (the time is not given). The analysis is carried out under the assumptions that the jet engines produce control moments  $m_x$ ,  $m_y$ , and  $m_z$  about the principal axes of inertia of

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ACCESSION NR: AP4043292

the body and that with the expenditure of fuel the moments of inertia of the body do not change. In the first case, to determine the law of variation of  $m_x$ ,  $m_y$ , and  $m_z$  under which the angular velocity components  $\omega_x$ ,  $\omega_y$ ,  $\omega_z$  (in the article they are considered as phase coordinates) assume the prescribed values in the shortest time, the system of differential equations describing the rotary motion of the body and the system of differential equations for the phase impulses  $p_x$ ,  $p_y$ , and  $p_z$  are written. On the basis of the maximum principle of Pontryagin the optimal law for the variation of control moments is determined and the integration of the systems of equations is carried out. Integrals for phase coordinates and impulses are derived which make it possible to determine theoretically the optimal mode for braking the velocity of the body. On the basis of derived integrals it is established that the phase trajectory is a spiral space curve with a variable radius of curvature and a variable step, which winds around the  $\omega_z$ -axis. A similar procedure is used for determining the phase coordinates and phase impulses in the second case. From the analysis of the derived integrals it follows that in the first case all three control moments act in reverse until complete braking is achieved ( $\omega_x = \omega_y = \omega_z = 0$ ) and in the second case the transversal

Cord 2/3



ACCESSION NR: AP4043292

control moments  $m_x$  and  $m_y$  act alternately, while the longitudinal moment (in the direction of the axis of symmetry of the body) acts permanently until the longitudinal component of the angular velocity of the body becomes equal to zero. As a particular case, the elimination of the precession motion of the body when the longitudinal velocity component is constant is studied. The construction of phase trajectories is given. Orig. art. has: 2 figures and 51 formulas.

ASSOCIATION: none

SUBMITTED: 14Oct63

ATD PRESS: 3093

ENCL: 00

SUB CODE: PR, MA

NO REF SOV: 002

OTHER: 001

Card 3/3

ACC NR: AP6028317

SOURCE CODE: UR/0040/66/030/004/0625/0635

AUTHOR: Smol'nikov, B. A. (Leningrad)

ORG: none

TITLE: Motion of a solid body with rotating flywheels around the mass center

SOURCE: Prikladnaya matematika i mekhanika, v. 30, no. 4, 1966, 625-635

TOPIC TAGS: motion mechanics, solid body rotation, Volterra ~~problem~~ <sup>rotation</sup> ~~flywheel~~ ~~body~~

ABSTRACT: An analysis is made of the particular case of the Volterra problem (the problem of rotation of a solid body around the center of mass in the case when some stationary cyclic rotations which do not change the distribution of mass of the body are taking place inside the body) when the rotating solid body is dynamically axially symmetric and a system of flywheels rotating at constant velocity relative to the rotating body is placed inside the body. Under the assumption that the angular momentum of the system during the motion is constant (no external disturbing forces), a system of differential equations with the Euler angles  $\phi, \theta, \psi$ , as principal variables is written to describe the motion of the system and the energy integral is derived. From the equations of motion utilizing the energy integral, the following equation is derived:

$$\left(\frac{d \cos \theta}{dt}\right)^2 = -R^2 f_1(\theta) f_2(\theta), \quad (1)$$

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ACC NR: AP6028317

where  $f_1(\theta)$  and  $f_2(\theta)$  are particular functions important in analyzing the motion of a system. The results from an analysis of this equation revealed the geometry of the motion. The possible modes of motion of the system are indicated and their dependence on the parameters and initial conditions of the system are established. It is shown that the trajectory of the axis of symmetry of the body describes loop-like curves on the surface of a unit sphere similar to corresponding curves of the Lagrange problem. Orig. art. has: 56 formules. [LK]

SUB CODE: 20/ SUBM DATE: 27Sep65/ ORIG REF: 003/ OTH REF: 002/ ATD PRESS: 5058

Card 2/2 11b

S/169/62/000/007/069/149  
D228/D307

AUTHOR: Smol'nikov, B. M.

TITLE: Profiling by the method of mean gradients

PERIODICAL: Referativnyy zhurnal, Geofizika, no. 7, 1962, 32, abstract 7A211 (V sb. Razved. i promysl. geofiz., no. 41, M., 1961, 74-75)

TEXT: Equipment for the method of mean gradients is described. Its distinctive feature is the presence of two supplying and two receiving lines. The advantage of this equipment is that it is possible to measure the potential difference over a large profile interval without shifting the supply lines. [Abstracter's note: Complete translation.] ✓

Card 1/1

GOLOVTSYN, V.N.; SMOL'NIKOV, B.M.

Method of the charged body in the study of underground waters in  
the Crimean Mountains. Geofiz. sbor. no.7:153-154 '64. (MIRA 17:11)

1. Institut geofiziki AN UkrSSR.

SAPUZHAK, Ya.S.; SMOL'NIKOV, B.M.

Some features in the use of electric prospecting to study karsts  
in the Crimean Mountains. Geofiz. sbor. no.3:35-40 '62.  
(MIRA 15:9)

(Crimean Mountains--Karst) (Electric prospecting)

SMOL'NIKOV, B.M.

Efficient section of isooohms for electric prospecting maps.  
Geofiz. sbor. no.3:49-53 '62. (MIRA 15:9)  
(Electric prospecting—Maps) (Karst)

SMOL'NIKOV, B.M.

Depth of exploration in prospecting by curvilinear electric  
profiling. Geofiz.sbor. no. 5:68-70 '63.

Use of underground electric prospecting in cave exploration.  
Ibid.:71-74 (MIRA 17:5)

1. Institut geofiziki AN Ukr SSR.



SMOL'NIKOV, B.M. [Smol'nykov, B.M.]

Physicogeological conditions governing the geoelectrical study of  
karst phenomena in the Crimean Mountains. Dop. AN URSR no.7:  
959-961 '64. (MIRA 17:9)

1. Institut geofiziki AN UkrSSR. Predstavleno akademikom  
AN UkrSSR S.I.Subbotinym.

GOLOVTSYN, V.N.; IVANOV, B.N.; SMOL'NIKOV, B.M.

Some karstic and geophysical investigations of the runoff intake  
zones in the karsts of the Crimean Mountains. Geofiz. sbor. no.7:  
142-146 '64. (MIRA 17:11)

1. Institut geofiziki AN UkrSSR.

PRIVAL'SKIY, Boris Yakovlevich; SMOL'NIKOV, L.P., redaktor; KOVALENKO,  
N.I., tekhnicheskii redaktor.

[Automatic control of rolling mill electric drives] Avtomaticheskoe  
upravlenie elektroprivodami prokatnykh stanov. Sverdlovsk, Gos.  
nauchno-tekhn.izd-vo lit-ry po chernoi i tsvetnoi metallurgii, 1954.  
241. [Microfilm] (MLRA 8:5)  
(Automatic control) (Electric driving) (Rolling mill  
machinery)

POLTEV, Vladimir Kirillovich; SMOL'NIKOV, Lev Petrovich; SHPUNBERG, Ya.N.  
kandidat tekhnicheskikh nauk, retsenzent; KEL'NIK, V.P., redaktor;  
BELYAYEV, M.V., kandidat tekhnicheskikh nauk, redaktor; KOVALENKO,  
N.I., tekhnicheskii redaktor

[Electrical equipment for metallurgical shops] Elektrooborudovanie  
metallurgicheskikh tsekhov. Sverdlovsk, Gos. nauchno-tekhn. izd-  
vo lit-ry po chernoi i tsvetnoi metallurgii. 1954. 486 p. (MLRA 8:5)  
(Metallurgical plants--Electric equipment)

POLTEV, Vladimir Kirillovich; SMOL'NIKOV, L.P., redaktor; KEL'NIK, V.P.  
redaktor; KOVALENKO, N.I., tekhnicheskii redaktor.

[Electrician of the metallurgical shop] Elektrik metallurgicheskogo  
tsakha. Izd. 2-e, perer. i dop. Sverdlovsk, Gos. nauchno-tekhn.  
izd-vo lit-ry po chernoi i tsvetnoi metallurgii, Sverdlovskoe otd-nie,  
1955. 2<sup>1/4</sup> p. (MLRA 8:8)  
(Metallurgical plants--Electric equipment)

PHASE I BOOK EXPLOITATION

729

Poltev, Vladimir Kirillovich, and Smol'nikov, Lev Petrovich

Spravochnoye rukovodstvo elektriika metallurgicheskogo zavoda (Reference Manual for Electricians in Metallurgical Plants) Sverdlovsk, Metallurgizdat, 1955. 456 p. 17,000 copies printed.

Eds.: Zotov, N.P., Burde, L.V., and Krapivin, B.G.; Ed. of Publishing House: Kel'nik, V.P.; Tech. Ed.: Kovalenko, N.I.

PURPOSE: This monograph is addressed to electricians working in metallurgical factories.

COVERAGE: The book gives technical data and characteristics of electrical equipment and apparatus widely used in metallurgical plants. Practical information on the design, selection and operation of electrical equipment and apparatus is given. The book contains, in addition to general discussions of equipment, data on the operation, adjustment, and testing of such equipment and apparatus. In composing the book, the authors have taken into consideration the fact that at present there is being used in metallurgical plants equipment no longer produced by the electrical equipment

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SMOL'NIKOV, L.P.  
25(1) PHASE I BOOK EXPLOITATION SOV/1710

Poltev, Vladimir Kirillovich, and Lev Petrovich Smol'nikov

Elektrooborudovaniye osnovnykh tsekhov metallurgicheskikh zavodov  
(Electric Equipment of the Principal Shops of Metallurgical Plants)  
2nd ed., rev. and enl. Sverdlovsk, Metallurgizdat, 1957. 519 p.  
14,000 copies printed.

Ed.: L.A. Varnachev; Ed. of Publishing House: V.P. Kel'nik; Tech.  
Ed.: Ye.M. Zef.

PURPOSE: This is a textbook for schools and courses for master electricians in metallurgical plants. It may also be of use to engineers and technicians concerned with the operation of electrical equipment in metallurgical plants.

COVERAGE: The authors explain the theory of electric drives and describe operating principles and construction details of electric machines and apparatus of electric drives in metallurgical plants. They also describe automatic control systems for electric drives. This is the second edition of the book which has been revised and enlarged. The authors thank the power engineering personnel of

Card 1/1

SMOL'NIKOV, L. P., Cand Tech Sci (diss) -- "A method of developing systems of optimal control of the rate of rolling on reversing stands". Leningrad, 1959. 16 pp (Min Higher and Inter Spec Educ RSFSR, Leningrad Electrical Engineering Inst im V. I. Ul'yanov (Lenin)), 200 copies (KL, No 11, 1960, 134)



28.1000, 25.2000

77150  
SOV/148-59-9-20/22

AUTHOR: Smol'nikov, L. P. (Engineer)

TITLE: Concerning the Problem of an Optimal Control System  
for the Main Drive of a Reversing Mill

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Chernaya  
metallurgiya, 1959, Nr 9, pp 171-177 (USSR)  
2,

ABSTRACT: The author studies optimal conditions for the control  
of the main drive of a computer-equipped reversing  
mill. It is assumed that the control system for the  
main drive is an element of the automation complex  
of the rolling mill; consequently, rolling conditions  
which would ensure maximum productivity of the mill as  
well as the required quality of the rolled product at  
a given reduction had to be determined. The author  
investigated the following: (1) rational graphs of  
rolling speeds were studied experimentally as well  
as theoretically under the assumption that the control  
system of the main drive has been predetermined. The  
determination of the optimal rates of changes in rolling

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Control System for the Main Drive of  
a Reversing Mill

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where  $M_{\max}$  = maximum moment of motor in ton-m;  $M_c$  =  
= moment of static resistances equaling the sum of the  
rolling moment and the moment of idle motion of the  
mill in ton-m,  $GD^2$  = moment of inertia of the drive  
in ton-m<sup>2</sup>; (2) Speeds of bite ( $n_b$ ) and ingot ejection  
( $n_e$ ) have been discussed at numerous occasions,  
although no unanimous opinion prevails on the subject.  
For a rational selection of values  $n_b$  and  $n_e$  the  
author analyzes the limitations imposed by the power  
of the motor. The velocity graph for one pass is  
assumed to be trapezoidal. During the standstill  
the reversing occurs at speeds which change recti-  
linearly. Equivalent moment  $M_e$  is determined for  
one pass according to the equation:

$$M_e^2(t_m + t_0) = (M_c + M_a)^2 t_a + M_c^2 t_b + (M_c - M_b)^2 t_0 + M_{b_0} t_0. \quad (2)$$

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where  $M_a$ ,  $M_b$ ,  $M_{b_0}$  = dynamic moments during acceleration  
with ingot, slowdown with ingot, and reversing during  
standstill, respectively. By means of mathematical  
calculations and substitutions the speed of bite was  
determined as:

$$u_b = \left(1 + \frac{M_a}{M_c}\right)^2 u_n, \quad (8)$$

and the speed of ejection as

$$\eta_e = \frac{(M_c - M_b)^2 - 2u_n \frac{b}{t_0} \left(\frac{GD^2}{375}\right)^2}{M_c^2 + 2u_n \frac{b}{t_0} \left(\frac{GD^2}{375}\right)^2} u_n < \left(1 - \frac{M_b}{M_c}\right)^2 u_n. \quad (9)$$

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$$u_{ei} = f_1(\Delta h_i : B_i : D_{pi} : N_i) \quad (10)$$

Here  $\Delta h$  = reduction,  $B$  = width of ingot,  $D_p$  = working diameter of rolls,  $N$  = serial number of roll pass. Considering that  $t_o(i+1) = t_{sm}(i+1) = F(\Delta h_{i+1})$  the optimal speeds of ejection in passes without edging are expressed as follows:

$$u_{ei} = f_2(\Delta h_{i+1} : D_{pi} : p : k) \quad (11)$$

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a Reversing Mill

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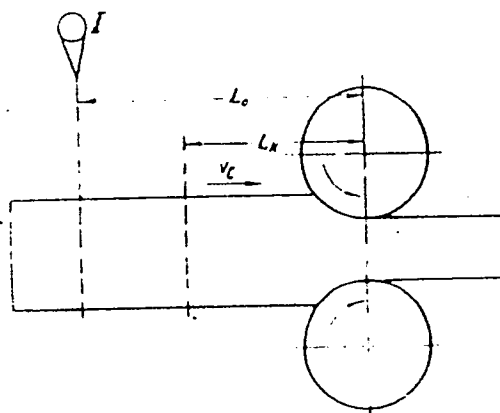


Fig. 2. Diagrammatic representation of a reversing mill: (I) indicator of position of metal; ( $L_k$ ) length of the ingot part which has not been rolled; ( $L_o$ ) distance between roll axes and indicator; ( $v_c$ ) speed of the rear of the ingot.

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a Reversing Mill

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so that the speed of the rolls equals  $n_0$  at the moment when the ingot returns to the rolls. By means of calculus of variations the author found that the rectilinear changes in the speed during the standstill correspond to a minimum heating of the motor. The character of the speed curve is suitable for purposes of automation; (4) Main drive requirements: the control system must allow slowdown with the ingot, and also reversing during the standstill with constant acceleration which can be predetermined. Acceleration with the ingot should be integrated in the speedup function so that a speedup rate permissible under conditions of the motor load would be ensured for each pass. The necessary estimation of the possible static load is done according to ingot temperatures or the load in the preceding pass. The rate of speedup in each pass can be programmed. In selecting parameters for the control system values  $\mu$  and  $\Delta t$ ,

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(  $\mu = \frac{\Delta t}{t}$  where  $\Delta t$  = time necessary for the setting

Concerning the Problem of an Optimal  
Control System for the Main Drive of  
a Reversing Mill

77150

SOV/148-59-9-20/22

of the predetermined deceleration slowdown in sec)  
should be decreased in order to facilitate operations  
as well as to diminish errors  $\delta_{n_e}$  and  $\delta_{n_b}$  ( $\delta_n =$   
maximum value of relative error). There are 4  
figures; and 6 Soviet references.

ASSOCIATION: Leningrad Electrotechnical Institute (Leningradskiy  
elektrotekhnicheskii institut)

SUBMITTED: April 17, 1959

Card 10/11

Concerning the Problem of an Optimal  
Control System for the Main Drive of  
a Reversing Mill

77150

SOV/148-59-9-20/22

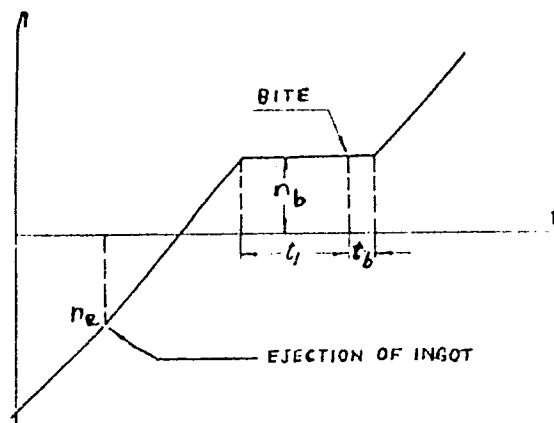


Fig. 4. Speed diagram of rolling during acceleration:  
( $n_b$ ) speed of bite; ( $n_e$ ) speed of ejection.

Card 11/11



PHASE I BOOK EXPLOITATION

SOV/4250

Smol'nikov, Lev Petrovich

4 Elektroavtomatika tekhnologicheskikh protsessov v metallurgicheskikh tsekhakh  
(Electric Automation of Manufacturing Processes in Metallurgical Plants)  
Sverdlovsk, Metallurgizdat, 1960. 207 p. Errata slip inserted. 3,150  
copies printed.

Reviewer: A. V. Fateyev; Ed.: B. N. Dralyuk; Ed. of Publishing House: V. P. Kel'nik;  
Tech. Ed.: R. M. Matlyuk.

PURPOSE: This book is intended for electricians at metallurgical plants and  
technicians working in automation laboratories in the metallurgical industry.  
It can also be useful to students specializing in automation at tekhnikums.

COVERAGE: The author examines special automation devices such as transducers  
and computers (both discrete and continuous) and other special apparatus used  
in automating metallurgical plants. He also discusses the automation of  
basic equipment used in blast furnaces, steel-making plants, and rolling mills.  
In compiling this book the author drew upon published literature and his own

Card 1/5

nasofaringealno obzračje in po avtomatizaciji proizvodstvenih procesov v kmetihostrojni in avtomatiziranemu elektroizvoru v promislenosti. Jd, Moscow, 1959

Doklady i izvestiya promyshlennyykh ustanovki, trudy soveshchaniya  
(Electric Drive and Automation in Industrial Systems) Transactions of the Com-  
ference) Moscow, Gosenergetizdat, 1960. 470 p. 11,000 copies printed.

General Eds.: I.I. Petrov, A.A. Strotin, and M.G. Chilikin; Eds.: I.I. Sol, and E.P. Silasov; Tech. Eds.: E.P. Voronin, and G.Ye. Lashinov.

**PURPOSE:** The collection of reports is intended for the scientific and technical personnel of scientific research institutes, plants and schools of higher education.

[illegible]

**PART. GENERAL PROBLEMS CONCERNING THE THEORY AND PRACTICE OF ELECTRIC DRIVE AND AUTOMATION OF CONTROL**

226	Metallurgical Practice <sup>6</sup>
227	Plasman, V.L., Doctor. Utilization of Gas-Tube Converters for Reversing Electric Drives
228	Imantsev, B.P., Doctor, Candidate of Technical Sciences. Electronic Regulation of Reversing Mill Drives
229	Dubinsk, B.B. and G.Y. Slonimsky, Engineers. "Bogach" Regulation System for Sheet Thickness on a Continuous High-Speed Cold-Rolling Mill
230	Shchegolev, I.M., Candidate of Technical Sciences. Automatic Stop Systems of the Cold-Rolling Reversing Mill 1200"
231	Alenkov, Y.D., Candidate of Technical Sciences. Electric Drives of Rolling Shafts
232	Domenchitskiy, G.M., Candidate of Technical Sciences. Problems of Designing an Optimum Control System for Rolling Shafts
233	Alivisov, A.M., Engineer. Electric Drive of a Cold-Rolling Mill Beel With an Aslatic Traction Regulation
234	Borzun, S.S., Candidate of Technical Sciences. Stabilizing Devices of Rolling Mill Electric Drives With Magnetic Amplifiers
235	Chaynikin, A.B., Candidate of Technical Sciences. Roughing Shop Automation With the Use of a Control Computer
236	Shchegolev, I.M., Doctor. Automatic Control of Rolling at Reversing Mills
237	Golovinskiy, V.P., Engineer. Automation of Mill 900 at the Ball-Structural Shop of the Ribnovo-Tselinok Metallurgical Plant (Ribnovo Tselinok Metallurgical Plant)

SMITH, L. P.

POLTEV, Vladimir Kirillovich; SMOL'NIKOV, Lev Petrovich; VARNACHEV,  
L.A., red.; KRYZHOVA, M.L., red.izd-va; MATLYUK, R.M.,  
tekhn.red.

[Reference manual for electricians of metallurgical plants]  
Spravochnoe rukovodstvo elektriķa metallurgicheskogo zavoda.  
Izd.2., ispr. i dop. Sverdlovsk, Gos.nauchno-tekhn.izd-vo  
lit-ry po chernoī i tsvetnoi metallurgii, Sverdlovskoe otd-nie,  
1960. 511 p. (MIRA 13:12)  
(Metallurgical plants--Electric equipment)  
(Electricians--Handbooks, manuals, etc.)

SMOL'NIKOV, L.P., inzh.

Question on optimum conditions of velocity for automatically controlled reversing hot rolling mills. Izv. vys. ucheb. zav.; energ. 3 no.8: 27-34 Ag '60. (MIRA 13:9)

1. Leningradskiy elektrotekhnicheskiy institut imeni V.I. Ul'yanova (Lenina). Predstavlena kafedroy avtomatiki i telemekhaniki.  
(Rolling mills) (Automatic control)

30480  
S/146/61/004/005/005/011  
D221/D305

16.8000 (1031, 1103, 1329)

AUTHORS: Balkani, D. and Smol'nikov, L.P.

TITLE: Calculating the tuning parameters for a relay regulator with a rigid feedback, operating in intermittent conditions

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Priboro-stroyeniye, v. 4, no. 5, 1961, 66-75

TEXT: An analysis is given of the intermittent operation of a relay controlling slow processes, the arrangement of which is shown in Fig. 1. The object of its control K, is an aperiodic link of the first order with a time constant  $T_1$ , for regulating the parameter  $\theta$ . The control organ CO is actuated by an executive organ EO having a constant speed of rotation. The regulator consists of a relay amplifier P and measuring bridge M. The chopper C switches in the regulator periodically. The author formulates initial equations, considering the chopper as closed, and assuming that the time

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Calculating the tuning...

constant of the executive organ and of it is smaller than  $T_k$ . To determine the increment of parameter  $\Delta\theta_{sr}$  it is assumed that  $\theta = \theta^0_{s.r}$  when there is not control. The value of  $\Delta\theta_i$  which characterizes the lack of sensitivity (i = insensitivity) of the regulator is given by  $\Delta\theta_i = \frac{k}{K + K_c} \cdot \frac{U_{sr}}{K_n}$ . This is followed by analy-

sis of step changes in the exciting agent. After mathematical elaborations a set of equations is deduced for the relay function,  $F(z)$ , where  $z = x + \gamma \frac{dx}{dr}$ , and  $x = \frac{\Delta\theta - \Delta\theta_n^0}{\Delta\theta_n}$ ,  $\gamma = \frac{t}{T_k}$ . The automatic

control system is then analyzed with the aid of a three-chart phase plane. In case of thermal energy and chemical objects,  $\Delta\theta \ll \theta_k$ , and therefore,  $x \ll \xi$ , as well as  $y \ll \xi$ . Consequently, it is possible to make the approximation  $\frac{dx}{dy} = 0$ , and then the phase traj-

ectories in charts II and III are vertical lines. Equations of lines on which phase trajectories pass from one chart to another

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Calculating the tuning...

S/146<sup>30180</sup>/61/004/005/005/011  
D221/D305

are deduced. Two diagrams of point transformation are given which permit analysis of the automatic control for various initial conditions (one diagram is for closed chopper, the other for interrupting operation of the regulator). Possibilities of a damped transition process and self-oscillations are discussed. The diagram of point transformation allows calculation of the period and plotting the transition process in the case of a step change in the disturbing effect. This article was recommended by the Kafedra avtomatiki i telemekhaniki (Department of Automation and Telemechanics). There are 5 figures and 3 Soviet-bloc references.

ASSOCIATION: Leningradskiy elektrotekhnicheskii institut im.  
V.I. Ul'yanova (Lenina) (Leningrad Electrotechnical  
Institute im. V.I. Ul'yanov (Lenin))

SUBMITTED: March 8, 1961

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30480

S/146/61/004/005/005/011  
D221/D505

Calculating the tuning...

Fig. 1. Block diagram of the automatic control system: M - measuring bridge; 2 - chopper; 3 - relay; 4 - executive organ; 5 - control organ; 1 - control object; 6 - measuring instrument.

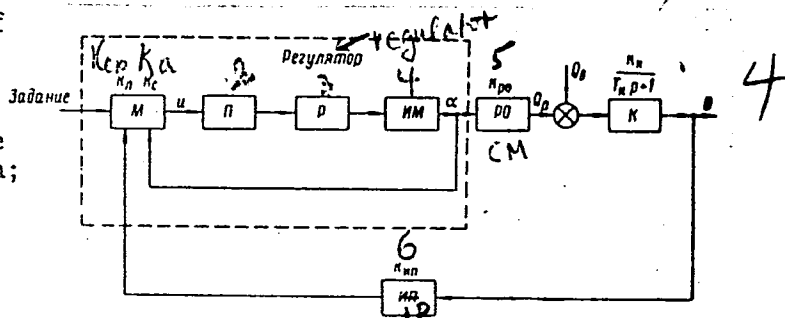


Рис. 1. Структурная схема системы автоматического регулирования:  
М - измерительный мост; П - прерыватель; Р - реле; ИМ - исполнительный механизм;  
РО - регулирующий орган; К - объект регулирования; ИП - измерительный прибор

Card 4/4



SMOL'NIKOV, LEV PETROVICH, kand.tekhn.nauk, assistant

Use of nonunitary feedback in designing optimum control systems  
for electric motors. Izv. vys. ucheb.zav.; elektromekh. 4  
no.7:41-49 '61. (MIRA 14:7)

1. Kafedra avtomatiki i telemekhaniki Leningradskogo  
elektrotekhnicheskogo instituta.  
(Electric motors) (Automatic control)

S/194/62/000/012/037/101  
D201/D308

AUTHOR: Smol'nikov, L. P.

TITLE: Determination of the appropriate rate of ingot ejection from the rollers in automatic reversible machine rolling

PERIODICAL: Referativnyy zhurnal, Avtomatika i radioelektronika, no. 12, 1962, 80, abstract 12-2-160 s (Izv. Leningr. elektrotekhn. in-ta, no. 46, 1961, 118-127) ✓

TEXT: In order to obtain maximum productivity of a reversible machine in automatic rolling the duration of operation of clamping arrangement, the return time  $t_0$  of the ingot ejected from the rollers for the next passage and the reversing time of the machine drive must be equal to each other. The dependence of  $t_0$  on the rate of ejection  $n_b$  of ingots from the rollers was investigated on a 1500 mm blooming and a 900 mm clamping bench. It was established

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Determination of the ...

S/194/62/000/012/037/101  
D201/D308

that  $t_o = k_o n_b$ , where  $k_o$  - a coefficient of proportionality depending on the sliding friction coefficient of metal against the roll train and on the working diameter of the rollers. In blooming rolling of 300 x 320 mm ingots,  $k_o$  for various passages differs from the mean value by not more than  $\pm 2$  to 3%. For establishing the dependence between  $t_o$  and  $n_b$  it is possible to use the values of  $k_o$  as determined for the rolling cycle as a whole. There is a correlation between  $t_o$  and  $n_b$ , its coefficient being 0.88. The suitable rate of ingot ejection is determined for the  $i$ -th passage by the expression  $n_{bi} = k_{ca} \sqrt{\Delta h_{i+1} / k_o}$ , where  $k_{ca}$  is a constant coefficient characterizing the performance of the clamp;  $\Delta h$  - the value of clamping force. From this expression, in which  $k_o$  has the experimentally determined value, the rate of ejection may be evaluated beforehand and introduced into the automatic process as a program, or it may be found automatically during the rolling process.

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Determination of the ...

S/194/62/000/012/037/101  
D201/D308

cess.  $k_0$  can change during the working process and requires, therefore, automatic adjustment. 2 figures. 2 tables. 4 references. (Abstracter's note: Complete translation. 7)



Card 3/3

BRAZHNIKOV, Nikolay Vasil'yevich; BONDARENKO, Vladimir Ivanovich;  
CHISTOV, Villen Petrovich; DRALYUK, B.N., retsenzent;  
SMOL'NIKOV, L.P., red.; BUR'KOV, M.M., red. izd-va; KOROL',  
V.P., tekhn. red.

[Automatic control of blast furnace and rolling mill processes with use of digital computers] Avtomatizatsiia domennogo i prokatnogo proizvodstva s primeneniem tsifrovyykh schetno-reshaiushchikh ustroystv. Sverdlovsk, Metallurgizdat, 1962.  
256 p. (MIRA 15:12)

(Blast furnaces) (Rolling mills)  
(Electronic digital computers)

SMOL'NIKOV, L.P., dotsent

Optimum relative switching duration for the electric drives  
mechanisms of rolling mills. Izv. LETI no.47:171-180 '62.  
(MIRA 16:12)

POLTEV, Vladimir Kirillovich[deceased]; SMOL'NIKOV, Lev Petrovich,  
CHAPAYKINA, F.K., red.i zd-ra; MIKHAYLOVA, V.V., tekhn.red.

[Electrical equipment of the main departments of metal-  
lurgical plants] Elektrooborudovanie osnovnykh tsekhov me-  
tallurgicheskikh zavodov; posobie dlia podgotovki masterov.  
Izd.3., ispr. i dop. Moskva, Metallurgizdat, 1963. 595 p.  
(MIRA 16:10)

(Iron and steel plants--Electric equipment)

SMOL'NIKOV, L.P. (Leningrad); BYCHKOV, Yu.A., (Leningrad); VOLKOV, Ye.F.  
(Leningrad)

Study of a ~~third-order~~ automatic control system optimum in  
respect to the sense of braking time with stabilized speed.  
Izv. AN SSSR. Tekh. kib. no.5:157-163 S-O '63. (MIRA 16:12)



SMOL'NIKOV, L.P. (Leningrad); KOTCHENKO, F.F. (Leningrad)

Automatic control system optimum in respect to response time with  
an asynchronous executive motor. Izv. AN SSSR. Tekh. kib. no.6:  
46-53 N-D '63. (MIRA 17:4)

ACCESSION NR: AR4014682

S/0271/64/000/001/A025/A025

SOURCE: RZh. Avtomatika, eleemekhanika i vy\*chislitel'naya tekhnika, 1964, no. 1, Abs. 1A168

AUTHORS: Balkani, Derd', and Smol'nikov, L. P.

TITLE: Approximate diagram of point transformation and its use for the study of relay control of slow processes

CITED SOURCE: Izv. Leningr. elektrotekhn. in-ta, vy\*p. 48, 1963, 212-226

TOPIC TAGS: automatic control, relay control, slow process, slow process, control, adaptive control system, self-adaptive control system, relay control system, automatic control system

TRANSLATION: A self-adaptive control system (SCS) is examined consisting of 1) a relay control (R) having a constant-rate regulator and a rigid feedback and 2) an object described by an equation which holds for an aperiodic unit with a long time constant. Equations are derived for describing SCS operation, and the operation is then investigated in terms of a three-sheeted phase plane. Simplified phase trajectories are drawn for slow processes. An approximate diagram of the

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ACCESSION NR: AR4014682

point transformation is constructed and used to find the motion of the system for various initial conditions. Together with the usual (single point) mode of R operation, multipoint modes are studied in which a single R is used to control a number of objects. In this case the R operates intermittently. This mode of operation is also studied with the aid of the point transformation diagram. Conditions are determined under which self-oscillation occurs, and parameters are found for the limit cycle. When relay delay is considered, the region of the initial conditions under which self-oscillation occurs becomes larger. Relations are obtained for calculating the tuning of the R which assures a tolerable static control error and an appropriate transient process. Orig. art. has 6 figs. and 3 refs.

A. L.

SUB CODE: GE

ENCL: 00

DATE ACQ: 19Feb64

Card 2/2

S/146/63/006/001/002/014  
D201/D308

AUTHORS: Balkani, D. and Smol'nikov, L. P.

TITLE: Calculation of tuning parameters of a multi-point proportional relay regulator for an object with delay

PERIODICAL: Izvestiya vysshikh uchebnykh zavedeniy. Priborostryeniye, v. 6, no. 1, 1963, 27-37

TEXT: Assuming a slow-varying process, the authors analyze the performance of a proportional relay regulator of an object represented by an aperiodic element with delay for the case of a single- and multi-point control state. The design of the regulator is deduced from a three-sheeted phase plane and an approximate diagram of the conformal mapping. The expressions derived give the conditions of stability, damped and natural oscillations of the system. Conclusion: the phase plane method should be used for the analysis of the motion of an automatic control system when it is necessary to take into account the limited positioning of the regulating element. There are 4 figures.

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Calculation of tuning ...

S/146/63/006/001/002/014  
D201/D308

ASSOCIATION: Leningradkiy elektrotekhnicheskiy institut im. V. I.  
Ul'yanova (Lenina) (Leningrad Institute of Electrical  
Engineering im. V. I. Ul'yanov (Lenin))

SUBMITTED: April 24, 1962

Card 2/2

BR

ACCESSION NR: AP4039388

S/0144/64/000/005/0527/0537

AUTHORS: Smol'nikov, Lev Petrovich (Candidate of technical sciences, Docent)

TITLE: On the application of the invariance principle to the synthesis of correcting devices for automatic regulation systems

SOURCE: IVUZ. Elektromekhanika, no. 5, 1964, 527-537

TOPIC TAGS: automatic control design, automatic control theory, automatic regulation, frequency response characteristic, compensating network

ABSTRACT: An algebraic method is proposed for the synthesis of correcting networks, suitable for automatic systems with complicated structural block diagrams, where the method of logarithmic frequency response functions cannot be readily used. If the transfer function of the automatic system is

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ACCESSION NR: AP4039388

$$K(p) = \frac{x(p)}{z(p)} = \Phi(p) \cdot \frac{1}{F(p)} = \frac{b_0 + b_1 p + b_2 p^2 + \dots}{a_0 + a_1 p + a_2 p^2 + \dots}$$

and the error signal transform is

$$\Phi_e(p) = \frac{\varepsilon(p)}{z(p)} = K(p) - 1 = \frac{(b_0 - a_0) + (b_1 - a_1)p + (b_2 - a_2)p^2 + \dots}{a_0 + a_1 p + a_2 p^2 + \dots}$$

then the synthesis of an equivalent corrected system (with minimized error) reduces to an evaluation of certain invariance coefficients, which are determined from the coefficients of the numerator and denominator of the transfer function  $K(p)$ . The procedure for determining the coefficients is indicated and the method is employed, by way of an example, to synthesize a parallel correcting network. The choice of the transfer function to satisfy certain quality indices is illustrated, and a numerical example is given. Orig. art. has: 5 figures, 21 formulas, and 1 table.

Card 2/3

ACCESSION NR: AP4039388

ASSOCIATION: None

SUBMITTED: 30Nov61

DATE ACQ: 19Jun64

ENCL: 00

SUB CODE: IE

NR REF SOV: 002

OTHER: 000

Card 3/3



KOTCHENKO, F.F. (Leningrad); SMOL'NIKOV, L.P. (Leningrad)

Optimal control of an automatic system with nonlinear  
mechanical characteristic of the servo motor. Avtom. i  
telen. 26 no.11:2051-2053 N '65.

(MIRA 18:12)

1. Submitted January 14, 1965.

ACC NR: AP7000285

(A)

SOURCE CODE: UR/0143/66/000/011/0090/C093

AUTHORS: Smol'nikov, L. P. (Candidate of technical sciences, Docent); Solonov, V. G. (Engineer); Volkov, Ye. F. (Engineer); Bychkov, Yu. A. (Engineer)

ORG: Leningrad Electrical Engineering Institute im. V. I. Ul'yanov (Lenin)  
(Leningradskiy elektrotekhnicheskii institut)

TITLE: An optimal digital servo system

SOURCE: IVUZ. Energetika, no. 11, 1966, 90-93

TOPIC TAGS: servosystem, optimal automatic control, rolling mill, digital system, electric motor, trigger circuit, magnetic amplifier, electronic feedback, second order differential equation / DP-42 electric motor

ABSTRACT: A brief description of a digital servo system for automatic control of the clamping device on a sheet rolling mill is presented. The servo system (see Fig. 1) uses an electromagnetic shaft position-to-digital converter (SDC) as the pickup of the true position of the upper roller B. An arithmetic device (AD) continuously calculates the difference  $\epsilon = A - B$  between the assigned position of the upper rollers A and B. The positive or negative difference (obtained in binary code) is converted to a voltage proportional to this difference by code-to-voltage converters (CVC). Near-to-optimum response speed of the system can be achieved by using strong linear motor-speed feedback. An experimental study performed directly on a mill

Card 1/2

UDC: 62-503.53

L 6992-66

ACC NR: AP5026807

SOURCE CODE: UR/0286/65/000/017/0090/0090

INVENTOR: Moin, V. S.; Nezhdanov, I. V.; Smol'nikov, L. Ye.; Laptev, N. N. 35

ORG: none B

TITLE: A semiconductor switch. Class 42, No. 174434

SOURCE: Byulleten' izobreteniy i tovarnykh znakov, no. 17, 1965, 90

TOPIC TAGS: semiconductor device, electric switch

ABSTRACT: This Inventor's Certificate introduces a semiconductor switch based on a  $p-n-p-n$  structure. Switching time from the "on" to the "off" state is reduced by connecting a diode between the  $n$ -regions with the anode connected to the  $n$ -emitter and the cathode connected to the  $n$ -base, while a second diode is connected between the  $p$ -regions with the anode connected to the  $p$ -base and the cathode connected to the  $p$ -emitter.

SUB CODE: EC/ SUBM DATE: 29Apr62/ ORIG REF: 000/ OTH REF: 000

Card 1/2

UDC: 681.142.07

L 6992-66

ACC NR: AP5026807

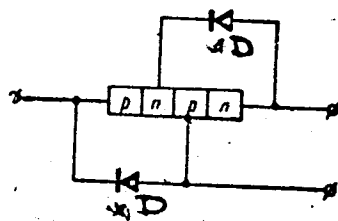


Fig. 1.

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